



Numerical and Experimental Vibration Studies of A Compact Vehicle Shell

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Abstract: This work deals with the numerical and experimental investigation of the free vibration properties of the shell compounds of a destroyed cylinder. Experimental setup and sample testing method demonstrated. The process of building the shell has also been described. Natural frequencies were determined using a programmable computer in the Mat lab environment based on the finite element method (OMM). The results are compared using the current formula with the existing literature. In addition, experimental values and numerical forecasts were compared using FEM. The effects of a percentage reduction on the natural frequency of the missile were studied. The effects of different parameters, i.e. curvature, boundary area, layer throwing, and aspect ratio on vibration interaction, were discussed for different boundary conditions.

Keywords: Delimitation Composite Plate Fundamental Frequency Woven Roving Glass-Epoxy Finite Element.

1. INTRODUCTION:

Composite materials are often used in various applications such as aerospace fields; airport domed roofing structures, nuclear fields, automotive industries, petrochemicals, and industrial industries. Features, etc. The strength, rigidity and aesthetics of shell panels are the highest priority in modern engineering applications due to their ability to meet design criteria [1]. Due to its unique strict structured benefits, curved laminate panels have been widely used in aviation industries such as the use of fuselage, wings, etc., where structures are most commonly used. Shell members are often used in modern Ural structural design applications. A good understanding of the mechanical behavior of the composite shell is important to ensure the integrity of these structures throughout the service life.

But there will be a limit to mixing plates during construction (such as partial wetness, or air trapping) or during service life (such as low speed, bird attack effect). They may or may not be visible on the surface, as they are contained within composite structures. However, the presence of boundary limits can significantly reduce the strength and rigidity of the structures and may also affect certain design parameters such as the shaking qualities of the structure (for example, the natural frequency and frequency). This is because the desired performance can be achieved by controlling the direction of the chip and the stacking order can alter its strict structural features, leading to a favorable design. Because the consistency of structures and yes. The consistency is greatly influenced by the presence of boundary in the coated curved plate, a comprehensive

understanding of the boundary behavior is more important to assess the Ural structural performance of the finite alloys. Shell members with defined borders can make significant changes to their dynamic properties [2][3]. So it plays an important role in the strict structural part from the design side. Therefore, it is important to study the effects of demarcation in a complex envelope.

II. DETEMINATION OF MATERIAL CONSTANTS

A complex plate behaves like a bone plate, whose properties can be defined by physical stability, i.e. E1, E2 and G12 plates have eight layers to estimate their properties. The 1195 UTM instrument was used to perform a tensile test on 45o vertical, transverse and longitudinal samples as defined in ACSM D3039 / D3039m (2008) standard. Stress test samples have a continuous, rectangular cross-section in all cases. Sample sizes are given in **Table 1** below.

Length(mm)	Width(mm)	Thickness(mm)
250	25	2.62

Table 1: Size of the specimen for tensile testing



To measure the modulus of the method, the specimen was loaded at a loading rate of 0.2 mm / min in an Instrument 1195 UTM (shown in Figure 6). The samples were first fixed on the upper jaw and then placed on the transferred jaw (lower jaw). It may be possible to prevent the sample from slipping too much. Here, it was taken as 50mm everywhere to make it richer. Initially the pressure was kept at the top. Along with the load, Spain was digitally recorded with the help of a load cell and scale extension. Figure 7. Example of a sample crack pattern during testing. From these figures obtained, the pressure curve is drawn against the stress and the initiator of the curve provides the coefficient of material to the young [4]. Using the axial sphygmomanometer, the length and lateral stresses are recorded and then the Poisson ratio is determined. The Poisson's ratio of the mixture for this study is 0.25.

III. EFFECTS OF CURVATURE:

To study the effects of the curve on the vibratory properties of the compound shell, three different types of samples were cut, the turning radius $R_1 = 0.91m$, $R_2 = 1.2625m$ and $R_3 = 2.09m$. Engineering and physical properties are provided as above. The numerical and experimental ratios of each of the laminated composite panels at the boundary position of O-O-A-A are shown in Fig. 23. Likewise, the natural frequency of three different radials of bends is 0.91m, 1.2625m and 2.09m.

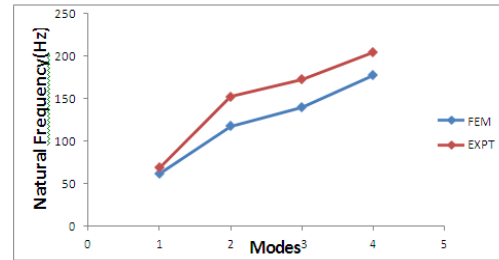


Fig 1 Variation of natural frequencies of laminated composite plate with modes.

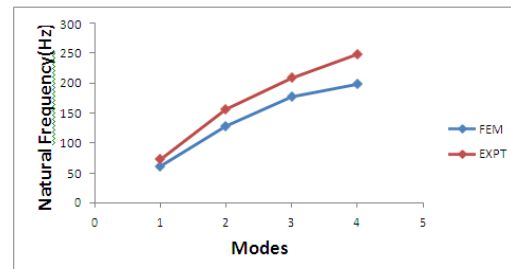
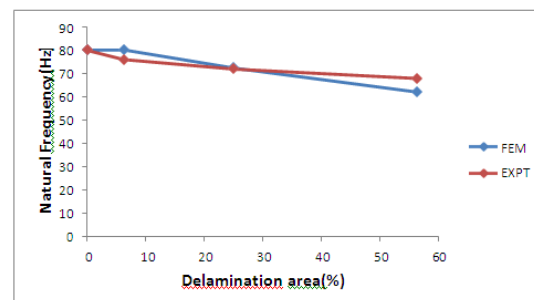


Fig 2 Variation of natural frequencies of laminated composite shell (R=0.91m) with Modes.

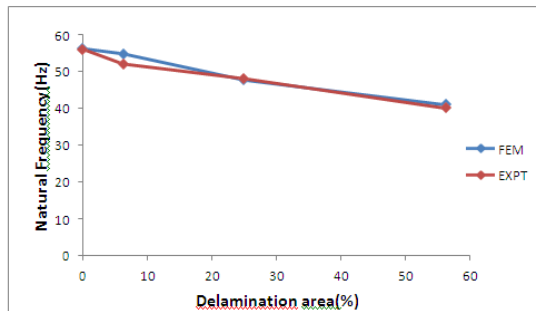
EFFECTS OF DELAMINATION AREA:

The effects of percentage determination on the vibration properties of the eight-layer composite projectile were studied by initiating the results at 6.25%, 25% and 56.25% of the sample area. Figure 27 shows the minimum common frequency of laminate complexes with boundary conditions free of charge on all four sides as a function of boundary field [5]. The experimental core frequencies were found to decrease from 6.25%, 25%, and 56.25% of laminate shells to 5%, 10% and 15%, respectively, when compared to the laminated shell. This may be due to the less rigidity of the pieces.



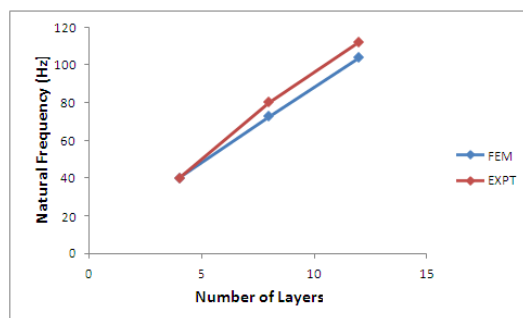
Subsequent authors offer Assisysafe (dependent and collaborate with two separate perspectives), attached to the CCC greeting boundaries, attached as Fig: 28 and Fig: 29. Workload of 6.25%, and basic building conditions realistic 25, 7%, 14% and 28% on

respectively for the boundary condition were 2%, 7.29% and 14.58% of the gravitational shell position of the CCC and 56.25% of the destructive shell, respectively [6]. This is supposed to be laminate from slices in the cafeteria.



EFFECTS OF NUMBER OF LAYERS OF LAMINATE:

To study the influence of the number of layers on the vibration behavior of a complex nest ant cylinder projectile with a 25% area determination, samples with 4, 8, and 12 pieces were prepared. The density of the sample is calculated at 1650 kg / m³ and 1627 kg / m³ for 4 layers and 12 layers, respectively. The numerical and experimental values of the natural frequency along with the number of layers are shown in Figure 30. From this graph, it appears that as the number of layers increases, the frequency of the shell increases as well. Also note that the frequency of the composite shell of the matrix shell increased by 8% for the four layers and 2 times and 2.8 times for the 12 layers, respectively. This result indicates that a relatively large number of layers have a significant positive effect on the hardening of the loose composite shell.



PULSE REPORT:

Natural frequencies of free vibration analysis were experimentally detected using the pulse program. Specific pulse reports are shown for a coated compound shell (1.0 a / b ratio and 25% of range). The listed FRFs provide different natural frequencies

from the best companies. The coordinates shown in refer to the measurement accuracy.

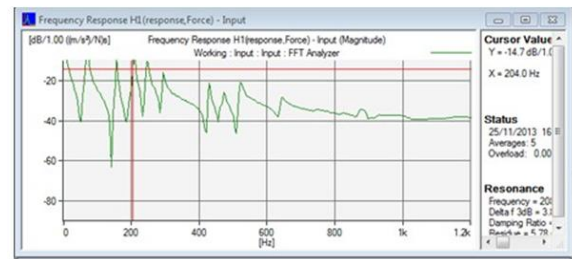


Fig 1: Frequency response function spectrum (In X-axis: Frequency in Hz, In Y-axis: Acceleration per force (m/s²)/N)

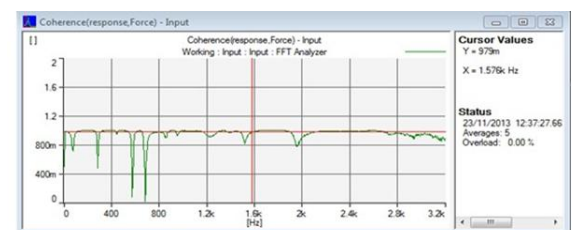


Fig 2: Coherence (Response, Force)

IV. CONCLUSION:

A detailed formulation is presented and a program is developed in MATLAB environment for the free vibration of delaminated composite shell. Both numerical predictions and experimental results on vibration of shell panels agree well. The natural frequency of shells increases as compared to plates due to curvature of panel. Due to decrease in radius of curvature to side ratio, the frequency of vibration of composite shell increases further. There is a decrease in natural frequency of composite shell with increase in percentage of delimitation irrespective of all the boundary conditions in woven fiber composite specimens due to reduction in stiffness. The fundamental frequency of cylindrical shell with fixed delimitation increases due to increase in number of layers due to bending stretching coupling. It is observed that there is an increase in vibration characteristic of composite shell with increase in aspect ratio.

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